

# AN INTEGRATED ADAPTIVE DISTANCE RELAYING SCHEME IN SERIES COMPENSATED TRANSMISSION LINES

S.G.SRIVANI and K.P.VITTAL

National Institute of Technology, Surathkal, Karnataka, India  
Ph.0824-2474000. Fax 0824-2474033, Email.-srivani\_9@hotmail.com, vittal\_nitk@yahoo.mail

**Abstract**— *The introduction of the capacitance in series with the line reactance adds certain complexities to the effective application of impedance based distance relays. The paper reviews series compensated line protection challenges and present modern solution to improve the distance relay performance. The work presents development and evaluation of an integrated adaptive distance protection scheme. Development of the proposed scheme is in the specific area of incorporating the Adaptive features like adaptive Relay setting as the compensation level changes in the series compensated lines of the transmission system for optimum reliability. Upon extensive testing on different data set of fault cases with fault resistance and varying percentage compensation level, performance of the developed method ensures that the proposed scheme overcomes the overreach / underreach problem of the distance relay in series compensated lines and is found to be quite promising.*

**Key words**—*Adaptive Distance Relay, Adaptive relaying scheme, Digital distance relay, Full Cycle Fourier Transform, Series compensation.*

## 1. Introduction

Series compensation plays the vital role in modern heavily loaded grid transmission lines. The series capacitor makes sense because it is simple and could be installed for 15 to 30% of the cost of installing a new line. Series compensation in modern power systems influences the power flow in particular network segment, reduces active power losses prevents system and sub synchronous oscillations, and connects more robustly different subsystems to stronger integrated network. The introduction of series compensation in existing networks requires not only extensive studies into the expected performance of the new system but also into the influence of its introduction on the operation of existing protection control and monitoring systems.

The protection of series compensated lines is considered to be one of the most difficult tasks. The protective distance relays, which make use of impedance measurements in order to determine the presence and location of faults, are "fooled" by installed series capacitance on the line when the presence or absence of the capacitor in the fault circuit is not known a priori.

The introduction of the capacitance in series with the line

reactance adds certain complexities to the effective application of impedance based distance relays. Series Capacitors(SCs) and their overvoltage protection devices (typically Metal Oxide Varistors (MOVs) and/or air gaps), in spite of their beneficial effects on the power system performance, introduce additional problems and make the operating conditions unfavorable for the protective relays that use conventional techniques and include phenomena such as voltage and/or current inversion, subharmonic oscillations, and additional transients caused by the air gaps triggered by thermal protection of the MOVs. The apparent reactance and resistance seen by the relay are affected due to the variation of series compensation voltage during the fault period.

As in all relaying, if the problem areas are anticipated and understood, the solution to the problem is achieved with comparative ease. In particular to series compensated lines the problems faced by the distance relay and some of the solution to these problems are researched and published.[1-7], Reach settings for the zones of protection with respect to some of the typical problems and adaptive approach have been discussed in [8]-[14]and [17]-[19]. Relay design progressing is concerned with the improvement of conventional relay algorithms based on phasor concepts. The complexities discussed in the protection performance of the series compensated lines call for the early fault detection and high-speed distance relays with good accuracy. We can find some of the advanced techniques with respect to the early fault detection and phasor estimation proposed in [20-24].

Adaptive reach settings of the distance relays for faults involving high arc resistance have been researched for some time now [23-25]. Methods for on-line corrections of the trip boundaries are presented using the wavelet transform in [26-28] and development of integrated protection systems in [29].

Despite constantly increasing power demand, series compensated lines are still quite rare. It is worth to undertake an effort to simulate transient conditions for series compensated applications, fine-tune and verify settings, and finally test the relaying system using digital simulators and/or play back systems.

*"In conclusion, the reach measurement can be singled out as the main source of problems for the protection of*

series compensated networks and still poses challenges to researchers. Hence, In view of the above issues and present power system scenarios, room to develop new adaptive techniques is open for research. Hence an attempt is made in this work to develop an Adaptive state of art scheme to meet the requirement of distance relay for optimum reliability in series compensated lines”.

## 2. Proposed distance Protection scheme

Considering the protection aspects of series compensated lines as discussed in the previous section, it is observed that an adaptive relay setting of the distance protection is required to cope up with the problems of overreach or underreach. Also it is deduced from the Literature review that the variations in the series compensation level are found to influence the apparent impedance measurements and trip boundaries. The apparent reactance and resistance seen by the relay are affected due to the variation of series compensation voltage during the fault period [1]-[6]. This serves as a basis of this proposed scheme.

The main idea behind the proposed solution is to have a typical digital distance relay scheme with extra information received from other local and remote relay. The relay changes its setting or action based on the received information. The concept of adapting the relay performance based on information from other relays is receiving much more acceptance because the speed of data transfer has increased and the expense of communication systems has declined

The proposed distance scheme is supplied off-line with detailed network information, e.g. length, impedance of each line in the concerned network. The relay operates normally as a typical digital distance relay. However, with the new information fed to the relay through the communication system, the relay performance will be changed based on this information. This information is received from the local and remote end relays. It includes:

- 1) Name of the faulty line
- 2) Series Compensation level
- 3) Value of running calculated impedance
- 4) Fault zone (one or two).

The work describes the development of an adaptive technique and the apparent impedance calculation procedure along with detailed simulation results for distance relaying schemes in which series capacitor comes in the fault loop of the transmission line considered.

The objectives of the work presented in the following section are

- 1) Development of an Adaptive relaying scheme for varied level of series compensation.
- 2) Simulation of series compensated system for the Fault data.

- 3) Distance computation for Zone 1, Zone 2 and the directional unit setting and development of Adaptive Relay logic.
- 4) Performance Evaluation of the Adaptive Relay of the proposed scheme.

Fig.1.depicts the procedural steps of the proposed scheme

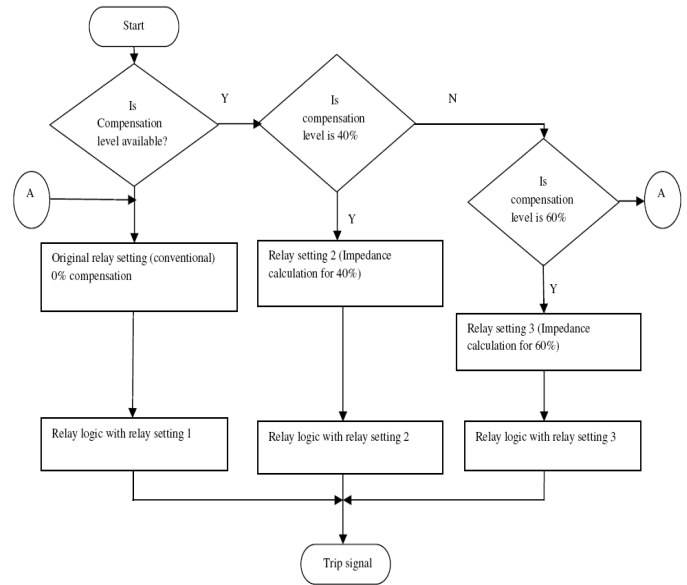


Fig 1. Sequence of proposed Adaptive Distance Protection Scheme

### A. Development of an Adaptive Scheme for varied level of series compensation

The proposed adaptive scheme, detailed in the Fig.1. first checks to confirm whether the series compensation level is available. The steady state characteristics of the relay are modeled for the three compensation levels like 0%, 40% and 60%. Depending on the availability of the compensation level, the relay adapts its setting accordingly. Then the dynamic characteristics of the relay are obtained using Full Cycle Fourier Algorithm (FCF) to check the status of the relay for the particular compensation level. The capacitance to particular compensation level will be used for faulted line impedance computation, but will not be used in healthy line's impedance calculation. Whenever the required information is not available, the proposed scheme uses the default setting as a conventional relay without the capacitor in the distance computation

### B. Simulation Of Series Compensated Transmission System For The Fault Data.

Figure 2, is the single line diagram of series compensated three phase transmission system model

considered for the simulation study [15] [16]. The realistic power system is simulated in MATLAB/SIMULINK platform. Figure 3 depicts the MOV protected series capacitor considered in the system.

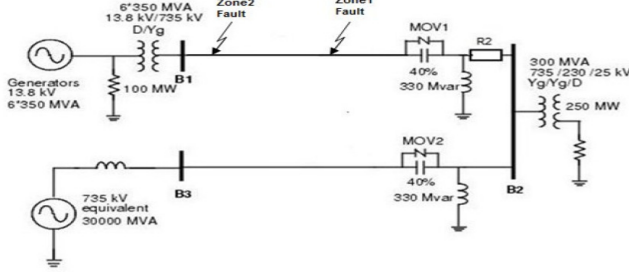


Fig.2. Series compensated transmission system model

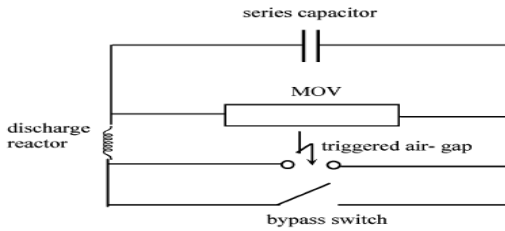


Fig.3 MOV protected series capacitor.

The details of the system simulated are as follows

- 1) The single-line diagram shown here represents a three-phase, 50 Hz, 735 kV power system transmitting power from a power plant consisting of six 350 MVA generators to an equivalent load system through a 600 km transmission line. The transmission line is split into two 300 km lines connected between buses B1, B2, and B3 as indicated in the system considered.
- 2) System has been initialized to 1500MW generation at 13.8KV bus. The parameters are measured at buses B1, B2 and B3.
- 3) Series compensation is done on transmission lines to increase the transmission capability of the system, the system is compensated and studied for different compensation levels like , 0%(conventional), 40% and 60% of the line reactance.
- 4) Line1 and Line2 are shunt compensated by 330MVar shunt reactance. Series capacitor banks on both the lines are similar. From the network shown we can observe that series and shunt compensation equipment is located at bus B2 station where load is applied. Transmission line inductance, capacitance and resistance considered are

$$L = 0.9337 \times 10^{-3} \text{ Henry / km}, \quad C = 12.74 \times 10^{-9} \text{ farad / km}$$

$$R = 0.01273 \Omega / \text{km}.$$

### C. Distance computation and Adaptive relay settings.

In First Zone Evaluation, due to the effect of subsynchronous oscillations caused by series capacitor,

during fault conditions the basic evaluation adjustment of the distance protection first zone should be reduced with respect to the conventional criteria, as it is detailed in Fig. 4 [8][9].

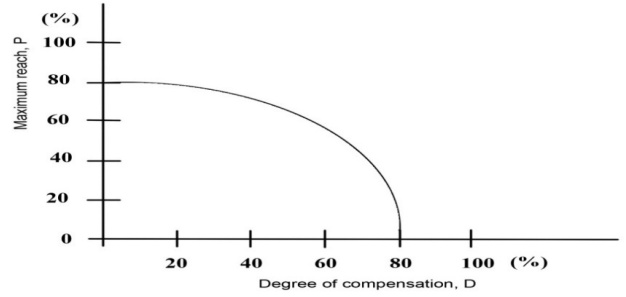


Fig. 4. First zone maximum reach as a function of the degree of compensation

"D", the degree of compensation of the line is defined as

$$D = \frac{X_L}{X_C} \times 100 \quad (1)$$

"Xc" and "XL" being the capacitor bank and the protected line reactance respectively. The 'p' value corresponds to the maximum permitted first zone reach, due to subsynchronous oscillations, as a percentage of the line impedance for a given value of "D". In the basic setting evaluation, considering compensated lines, the 'p' value is applied in both extremes to the difference given by fig. 4.

Table 1. 'P' value with respect to percentage compensation

$D = \frac{X_L}{X_C} \times 100$	'P' value
0	0.8
40	0.7
60	0.54

The reach setting used for simulation study is a parallelogram characteristic with a forward fault resistance of 10 ohm. The backward reach settings (directional unit setting) used are

$$R_b = -\frac{3}{5}(R_f) \quad (2)$$

$$X_b = -\frac{1}{2}(X_f) \quad (3)$$

Where  $R_b$  and  $X_b$  are backward resistance and reactance reach.

$R_f$  and  $X_f = X_{reach}$ , are their forward counterparts respectively.

The line impedane angle ( $\theta_L$ ) varies between  $84^\circ$ – $88^\circ$ . The calculated reach settings in perunit (pu) on

100 MVA base for the characteristic of the relay at all the three compensation levels are estimated and shown in the **Table 2** respectively.

Table 2. Reach setting of the adaptive Relay in perunit (pu)

Level of compensation	Zone 1 setting values in pu				
	$R_f$	$X_f$	$R_b$	$X_b$	$\theta_L$
0%	0.00555	0.0156	-0.00333	-0.0078	87.92
40%	0.00555	0.0082	-0.00333	-0.0041	86.54
60%	0.00555	0.0042	-0.00333	-0.0021	84.83
	Zone 2 setting values in pu (Conventional)				
	0.00555	0.0293	-0.00333	-0.0146	87.92

The steady state **Relay characteristic** obtained for the proposed adaptive scheme with the respective compensation level considered is shown in fig. 5. 0% compensation setting is considered as conventional relay characteristic. The Zone 1 and zone 2 reach characteristics for the conventional relay as obtained is shown in Fig.6.

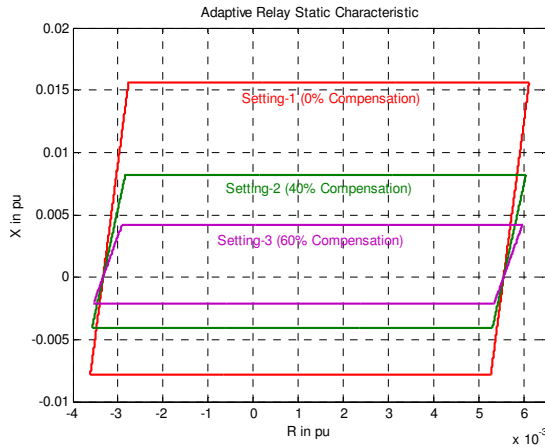


Fig.5 Adaptive Relay characteristic for Zone 1 w.r.t. level of compensation

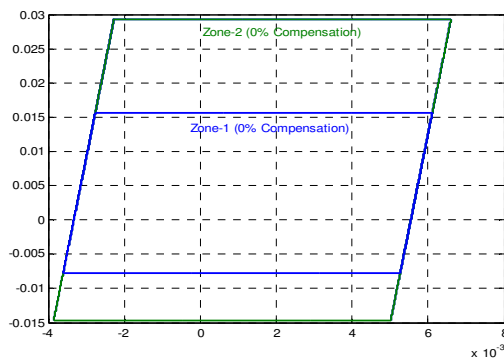


Fig.6. zone1 and zone2.of conventional Relay istic,

### C. Performance Evaluation of the Proposed Adaptive Scheme

1. Extensive simulation study is made on the series compensated transmission system (figure 1.6) for the faults like A-G, B-G, C-G, AB-G and ABC for each level of compensation.

2. The simulation study is made at a sampling frequency (Fs) of **6 kHz**. The performance evaluation is considered for the fore said faults with minimum inception angle and the fault resistance of 10Ω. The faults are applied on **Line 1**, on the **line side of the capacitor bank**. The measurement of fault signals for the relay **R2 are made at B2** substation.

3. Performance evaluation of **Relay R2** is made in detail as capacitor is in the fault loop .Two cases have been considered for the evaluation at all the three compensation levels.

1) *Case 1: Performance evaluation for the faults simulated within 80% of Line 1 length (in Zone 1).*

2) *Case 2: Performance evaluation for the faults simulated at 90% of the Line 1(in Zone 2 that is 10% outside Zone 1).*

4. For both the case study, fault is applied at t=1 cycle (0.01667 sec), and **4** cycles of post fault data signals are taken. Therefore at the end of the 5<sup>th</sup> cycle (at 0.083 sec) the breaker is open and the fault is eliminated at the 6<sup>th</sup> cycle.

5. For all the fault conditions as mentioned, data is recorded at a sampling time of 0.0001667 sec ( i.e. 100 samples/cycle)

Adaptive relay logic is developed in MATLAB considering the Full Cycle Fourier (FCF) algorithm for the fault impedance estimation. The relay logic adopted for its dynamic characteristic is developed. The impedance trajectories obtained for both the cases mentioned above are illustrated in respective figures according to their numbers , mentioned in the following tables of results. The figures clearly explain the need of such an adaptive scheme and the optimum performance of the proposed scheme in the modern power system scenarios.

The results of evaluation of the proposed adaptive relay are summarized and illustrated in **Table 3**, **Table 4** and **Table 5**. The Tables show the detail results of the fault conditions s of case1 and case2 for the three compensation levels respectively (0%, 40% and 60%). The results are shown in respect of operation in respective zones to overcome the problem of overreach/underreach (maloperation) of the relay and the operating time. To confirm the tripping .a trip counter is set for 5 samples for zone 1 and 100 samples for zone2 (delay time).The results discussion depicting the need and efficacy of this proposed scheme and the comparative analysis with that of conventional relay are detailed in the following section.

The results obtained illustrate the correct operation of the distance relay for the proposed scheme. The RX plots show that the relay adapts its characteristic to trip in the respective zones at all the three compensation levels according to the information received and the system condition (only plots of some sample cases are presented as indicated in the tables).

It is observed in simulation study that fault signals of AG fault at 40 % compensation, since a line-to-ground (AG) fault is applied and the fault current reaches 10kA, the MOV conducts at every half cycle and the energy dissipated in the MOV builds up to 13 MJ as shown in figure and stays constant at 13 MJ. As the maximum energy does not

exceed the 30 MJ threshold level, the gap is not fired. After  $t=6$  cycles the fault current drops to a small value and the line and series capacitance start to discharge through the fault and the shunt reactance. Hence the relay adapts to 40 % compensation characteristic settings.

Similarly it is also observed that during a three phase fault the energy dissipated in the MOV builds up faster than in the case of a AG fault, the energy reaches the 30MJ threshold level as a result the gap is fired and the capacitor voltage quickly discharges to zero through the damping circuit. Here, since the capacitance effect no longer exists, the relay can adapt to its conventional characteristic.

**Table 3. Results of evaluation for 40% compensation**

Type of fault	Location of fault	Fault signals Fig No.		R-X plot Fig No	R-T plot Fig No	X-T plot Fig No	Status of Relay ✓ Correct operation * mal operation (overreach)		Operating time in ms
		V	I				Conventional Relay	Adaptive Relay	
AG	Zone 1	7	8	11	12	13	✓	✓	16.67
	Zone 2	9	10	-do-	-	-	*	✓	31.306
BG	Zone 1	-	-	-	-	-	✓	✓	22.31
	Zone 2	-	-	-	-	-	*	✓	40.33
CG	Zone 1	-	-	-	-	-	✓	✓	18.17
	Zone 2	-	-	-	-	-	*	✓	43.66
ABG	Zone 1	-	-	-	-	-	✓	✓	23.33
	Zone 2	-	-	-	-	-	*	✓	44.83
ABC	Zone 1	-	-	-	-	-	✓	✓	21.00
	Zone 2	-	-	-	-	-	*	✓	41.01

**Table 4. Results of evaluation for 60% compensation**

Type of fault	Location of fault	Fault signals Fig No.		R-X plot Fig No	X-t plot Fig No	R-t plot Fig No	Status of Relay ✓ Correct operation * mal operation (overreach)		Operating time in ms
		V	I				Conventional relay	Adaptive Relay	
AG	Zone 1	-	-	14	-	-	✓	✓	22.57
	Zone 2	-	-	14	-	-	*	✓	47.51
BG	Zone 1	-	-	-	-	-	✓	✓	22.17
	Zone 2	-	-	-	-	-	*	✓	47.11
CG	Zone 1	-	-	-	-	-	✓	✓	27.00
	Zone 2	-	-	-	-	-	*	✓	48.84
ABG	Zone 1	-	-	-	-	-	✓	✓	21.56
	Zone 2	-	-	-	-	-	*	✓	43.01
ABC	Zone 1	-	-	-	-	-	✓	✓	21.83
	Zone 2	-	-	-	-	-	*	✓	43.51

**Table 5 Results of evaluation for 0% compensation**

Type of fault	Location of fault	Fault signals Fig No.		R-X plot Fig No	R-T plot Fig No	X-T plot Fig No	Status of Relay ✓ Correct operation * mal operation (overreach)	Operating time in ms
		V	I				Adaptive Relay/ Conventional Relay	
AG	Zone 1	-	-	15	-	-	✓	23.01
	Zone 2	-	-	15	-	-	✓	40.49
BG	Zone 1	-	-	-	-	-	✓	13.00
	Zone 2	-	-	-	-	-	✓	35.33
CG	Zone 1	-	-	-	-	-	✓	15.33
	Zone 2	-	-	-	-	-	✓	38.83
ABG	Zone 1	-	-	-	-	-	✓	15.83
	Zone 2	-	-	-	-	-	✓	43.34
ABC	Zone 1	-	-	-	-	-	✓	14.17
	Zone 2	-	-	-	-	-	✓	35.66
							✓	

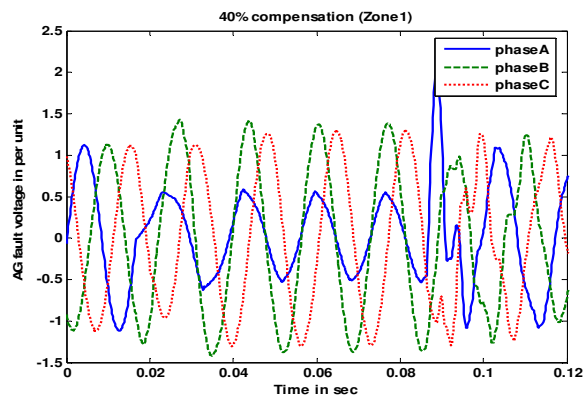


Fig7. AG fault voltage for case1 at 40% compensation

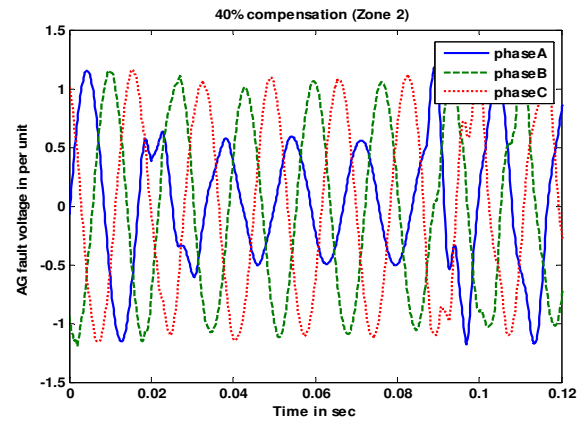


Fig 9 AG fault voltage for case2 at 40% compensation

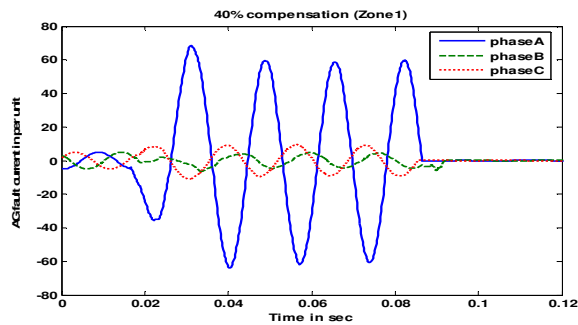


Fig 8 AG fault current for case1 at 40% compensation

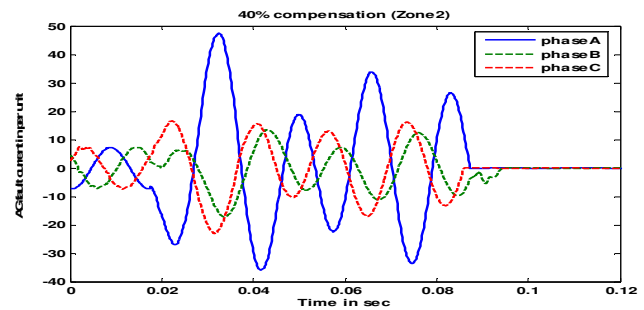


Fig.10 .AG fault current-case2-40% compensation

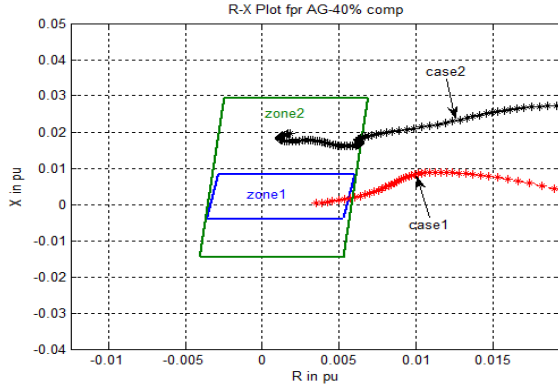


Fig.11. RX plot AG -case 1 and case 2-40% compensation

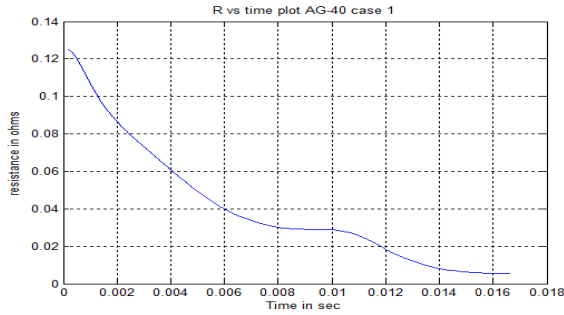


Fig.12 R Vs T plot for case 1 at 40% compensation

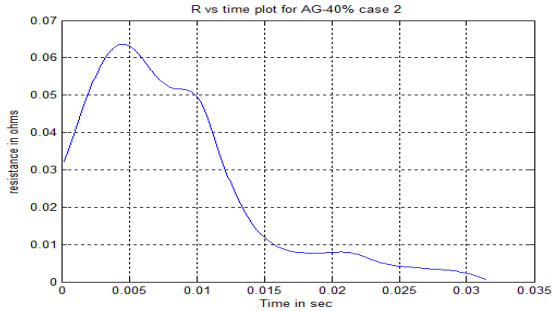


Fig.13. R Vs T plot for AG-case2 at 40% compensation

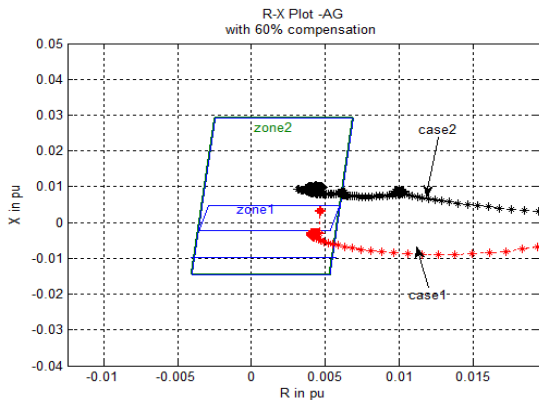


Fig.14. RX plot for case1 and case2 at 60% compensation

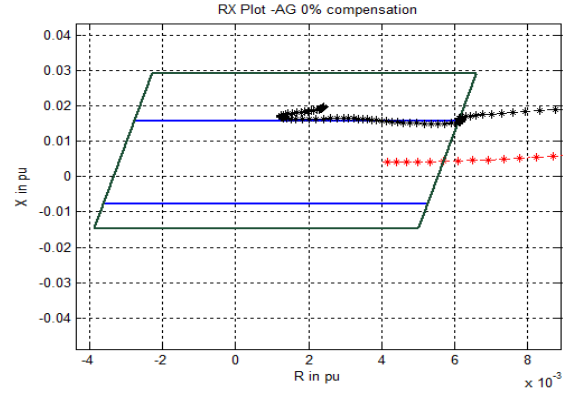


Fig.15. RX plot for case1 and case2 at 0% compensation

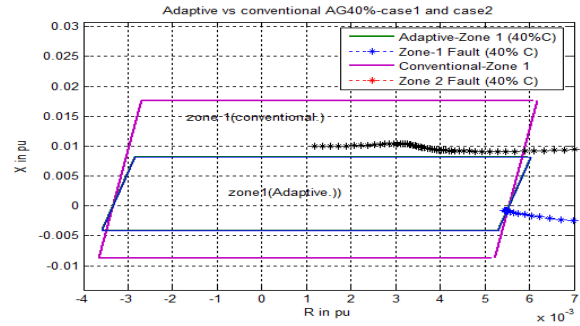


Fig.16 R X plot for Adaptive relay Vs Conventional relay for case1 and case2 at 40 % compensation

### 3. Conclusions

The results illustrate the correct operation of the distance relay for the proposed scheme. The RX plots show that the relay adapts its characteristic to trip itself in the respective zones for all the three compensation levels, according to the information received on the system condition, which the conventional relay is incapable of handling. In particular, we can observe overreaching problem in Figure 16 where the conventional relay trips in zone 1 for the fault in zone 2 where as the adaptive relay trips precisely in zone 1 only for the case1 conditions as indicated by the RX plot.

Extensive comparative analysis made here with conventional relay prove the need of the proposed scheme in series compensated lines for optimum protection.

### References

1. Stan Wilkinson, GE Power Management Ontario, Canada; "Series Compensated Line Protection Issues, GER 3972, pp 1-22.
2. Bogdan Kasztenny, "Distance Protection Of Series Compensated Lines -Problems And Solutions", *28<sup>th</sup> Annual western protective relay conference*, October, 2001, pp 1-34.

3. Goldsworthy D.L., "A linearized model for MOV-protected series capacitors", *IEEE Transactions on Power Systems*, Vol.2, No.4, pp.953-958, November 1987.
4. Novosel, D.; Phadke, A.; Saha, M.M.; Lindahl, S, "Problems and solutions for microprocessor protection of series compensated lines," *Developments in Power System Protection, Sixth International Conference on (Conf. Publ. No. 434)* , pp.18-23, 25-27 Mar 1997.
5. *CICRE, Working Group of Study Committee 34* , "Application Guide on Protection of Complex Transmission Networks", May 1991.
6. F. Anderson and W. Elmore, "Overview of Series-Compensated Line Protection Philosophies", *Western Relay Protective Conference*, Washington State University, Spokane, Washington, October 1990.
7. Clint T. Summers, "Distance Protection Aspects of Transmission Lines Equipped with Series Compensation Capacitors", Thesis September 29, 1999.
8. Rogelio A. Castro, and Pineda, H.A., "Protection System Considerations for 400 kV Series Compensated Transmission Lines of the Central Western Network in Venezuela," *Transmission & Distribution Conference and Exposition: Latin America, 2006. TDC '06. IEEE/PES* , pp.1-5, 15-18 Aug. 2006.
9. Asea Brown Boveri, "REL 531\*2.3 High speed line distance protection terminal". *ABB Publication IMRK 506 107-UEN*, pp. 54-105. Jul. 2001.
10. P.K. Dash, A.K. Pradhan, G. Panda and A.C. Liew "Digital protection of power transmission lines in the presence of series connected FACTS devices" 2000 *IEEE*, pp.1967-1972
11. Mojtaba Khederzadeh, T.S.Sidhu, "Impact of TCSC on the Protection of Transmission Lines", *IEEE Transactions on Power Delivery*, Vol.21, Jan 2006.
12. Ricardo Dutra, Fabiano L. Oliveira W, Saha M.M. and Lidstrom S. "Adaptive distance protection for series compensated transmission lines," *Transmission and Distribution Conference and Exposition: Latin America, 2004 IEEE/PES* , pp. 581- 586, 8-11 Nov. 2004.
13. Sidhu, T.S. Khederzadeh M, "Series compensated line protection enhancement by modified pilot relaying schemes," *Power Delivery, IEEE Transactions on* , vol.21, no.3, pp.1191-1198, July 2006.
14. Altuve, H.J.; Mooney, J.B.; Alexander, G.E.; , "Advances in series-compensated line protection," *Protective Relay Engineers, 2009 62nd Annual Conference for* , pp.263-275, March 30 2009-April 2 2009.
15. G. Sybille, Le-Huy and Hoang "Digital simulation of power systems and power electronics using the MATLAB/ SIMULINK Power System Blockset" *Power Engineering Society Winter Meeting, 2000, IEEE* ,Volume: 4 , 23-27 Jan. 2000 pp.2973 – 2981.
16. SimPower Systems : TransÉnergie Technologies User's Guide Version 3, The Math Works
17. A X. Jampala, S.S. Venkata and M.J. Damborg, "Adaptive transmission protection: Concepts and Computational issues", *IEEE Trans. on Power Delivery*. vol.4.No. 1.1989. pp. 177-185.
18. Z Zhtha, and C. Dcshu, "An adaptive approach in Digital Distance protection", *IEEE transaction on Power Delivery*, Vol. 6, No. 1, 1991, pp.135-142.
19. Y. Q. Xi & K. K. Li and A.K. David, Adaptive relay setting for standalone digital distance protection, *IEEE Trans. on Power Delivery*, Vol. 9, No. I, 1993, pp. 480-491.
20. De Oliveira, A.L.P.; da Silveira, P.M.; , "Evaluation of Distance Protection Performance applied on Series Compensated Transmission Lines using Real Time Digital Simulation," *Transmission & Distribution Conference and Exposition: Latin America, 2006. TDC '06. IEEE/PES* , 15-18, pp.1-6, Aug. 2006.
21. Saha, M.M.; Kasztenny, B.; Rosolowski, E.; Izykowski, J.; , "First zone algorithm for protection of series compensated lines," *Power Delivery, IEEE Transactions on* , vol.16, no.2, pp.200-207, Apr 2001.
22. Rosolowski, E.; Izykowski, J.; Kasztenny, B.; Saha, M.M.; "Differential equation based impedance measurement for series-compensated lines," *Electric Power Engineering, 1999. PowerTech Budapest 99. International Conference on* , pp.205, 1999.
23. Bin Su, Jianping Wang, Ying Yang, Weixing Gong, Yongsheng Xu,, "Setting Considerations of Distance Relay for UHV/EHV Long Transmission Lines," *Power Engineering Society General Meeting, 2007. IEEE* , pp.1-7, 24-28 June 2007.
24. Sadeh, J.; Ranjbar, A.M.; Hadsaid, N.; Feuillet, R.; "Accurate fault location algorithm for series compensated transmission lines," *Power Engineering Society Winter Meeting, 2000. IEEE*, vol.4, pp.2527-2532 vol.4, 2000.
25. P. K. Dash, S. R. Samantaray, and Ganapati Panda, "Fault Classification and Section Identification of Advanced Series-Compensated Transmission Line Using Support Vector Machine", *IEEE transactions on power delivery*, vol. 22, no. 1, January 2007, pp. 62-73.
26. Atif Saleem, S.M.; Sharaf, A.M.; , "A Novel Travelling Wave Based Relaying Scheme Using Wavelet Transforms for Arcing Faults Detection on Series Compensated Transmission Lines,"

- Electrical and Computer Engineering, CCECE 2007,proceedings Canadian Conference, April 2007*no, 22-26, pp.575-578.
27. S.R. Samantaray and P.K. Dash" Wavelet packet-based digital relaying for advanced series compensated line", *IEEE transactions.*, vol.1, no.5,2007, pp. 784–792.
  28. Chen, Z. Xiang-ning Lin, Bo, Z.Q. "Wavelet transform based boundary protection scheme for series compensated lines," *Developments in Power System Protection, 2004. Eighth IEE International Conference on*, vol no1, 15-8 April 2004, pp. 56-59.
  29. Bo Z Q, Dong X Z, He J H, Caunce B R J and Klimek A, "Integrated Protection of Distribution Network Using A New Directional Approach", *Fifth International Conference on Power Transmission &Network*, Beijing, October 2005

**S.G.Srivani** was born in Bangalore, in 1963. She received B.E (E&E).degree from Bangalore university, 1986, M.E. (power system) degree from Bangalore University in 1990, all from India. Presently working as Assistant professor in the department of Electrical and Electronics Engineering RVCE Bangalore and she is pursuing Ph D research program as part time research scholar at Dept. of Electrical & Electronics Engineering, NITK Surathkal, in India. She is a life member of Indian Society for Technical Education [ISTE]. She has published twelve technical research papers in various National and International conference proceedings .Her areas of interest include power system protection, signal processing, embedded systems and power quality.

**K. P. Vittal** was born in Bellary, Karnataka State, India in 1964. He received his B.E. (E & E) degree from Mysore University, in 1985, M.E. (Applied Electronics) degree from Bharatiar University, Coimbatore in 1989, and Ph.D. from Mangalore University, in 1999, all from India. Presently Dr.Vittal is serving as Professor at the Dept. of Electrical & Electronics Engineering, NITK Karnataka, India. He is member of IEEE, Life member of Indian Society for Technical Education [ISTE] and Institution of Engineers, India,[IE (India)].He has published 30 technical research papers in various National and International conference proceedings and two papers in Int. Journals. His areas of interest include Power System Protection, Distributed Generation systems, power quality and Design of Embedded Systems.