COMBINED SYSTEM OF STATIC VAR COMPENSATOR AND ACTIVE POWER FILTER FOR HARMONIC SUPPRESSION AND POWER FACTOR IMPROVEMENT

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Abstract: This paper presents a novel approach for power quality improvement in Power system. The proposed system consists of Static VAR compensator and shunt Active Power Filter (APF) for harmonic suppression, power factor correction and voltage stability. The system configuration and the control method for the Static VAR compensator are implemented using MATLAB-simulink software. An optimal non-linear PI controller is used to improve the performance of the Static VAR compensator and the Improved Generalized Integrator controller has been adopted to improve the performance of the APF. Moreover, the simulation results obtained for the non-linear system have been analyzed and reported.

Key words: Active power filter (APF), Static VAR Compensator (SVC), Improved SPX Algorithm, Harmonic suppression, Reactive power compensation

1. Introduction

Power quality problems are common in most of the commercial, industrial and utility networks. Harmonics and reactive power are two of the serious problems associated with the grid. They are caused by non-linear loads, including saturated transformers, arc furnaces, and semiconductor switches [1]. The presence of harmonics and reactive power in the grid is harmful, because it will cause additional power losses and malfunctions of the grid component.

The Shunt active power filter compensates current harmonics by injecting equal-but-opposite harmonic compensating current [3]. In this case the shunt active power filter operates as a current source injecting the harmonic components generated by the load but phase shifted by 180°. This principle is applicable to any type of load considered as a harmonic source. Moreover, with an appropriate control scheme, the load power factor can be compensating by active power filter.

To prevent the inflow of harmonic and reactive currents and to improve the operating ability of the transmission systems, a kind of Flexible AC Transmission System (FACTS) has been proposed. The Static VAR compensator (SVC) is an important component of FACTS. It usually installs in power transmission systems and serves in various ways to improve the system performance. By the rapid control of their reactive power output, the SVCs regulate system voltages, improve transient stability, correct power factor, reduce temporary over voltages, and damp synchronous resonances. Usually, an SVC is composed of a Thyristor-Controlled Reactor (TCR) and Fixed Capacitors (FCs). The FCs is often tuned in series with inductors to act as Passive Power Filters (PPFs) in the characteristic harmonic frequencies of the TCR.

2. System of SVC and APF

2.1 Configuration of the system

![Fig. 1. Configuration of the combined system](image-url)

The combined system comprises a classical SVC and an active filter with a coupling circuit. The SVC consists of delta connected TCR and star connected FC. The conduction angle δ of the TCR depends on the firing angle α. The relationship between δ and α is:

$$\delta = 2(\pi - \alpha)$$  \hspace{1cm} (1)

The firing angle α can be controlled to take any value between 90° and 180°, corresponding to the value of δ between 180° and 0°. The coupling circuit consists of inductor (L1) and capacitors (C1, CF) used for coupling the APF and the grid. L1 and C1 tuned at the
fundamental frequency and then compose the coupling circuit with \( C_F \). Moreover, its capacitor is in series with inductor to form single tune PPF. The APF in parallel with the fundamental resonance circuit is directly connected in series with a matching transformer. The coupling capacitor sustains fundamental sustains fundamental voltage of the grid, while APF only supports harmonic voltage, which greatly reduces the current requirements of APF and minimizes the voltage rating of semiconductor switching device. Because of these characteristics, the combined system is effective to suppress harmonics generated by both TCRs and nonlinear loads, to compensate reactive power dynamically, and to improve voltage stability.

3. Control method of SVC

The SVC mainly regulates system voltages and correct power factor. A non-linear PI controller is proposed to improve the dynamic response, decrease the overshoot of transient response and decrease the steady-state error of SVC. The \( K_p \) and \( K_i \) values of the non-linear PI controller is optimized using the Simplex algorithm.

3.1 Non-linear function

The non-linear function of the PI controller is given by:

\[
K(e) = 0.001 - \frac{2e^{0.05\pi \sin(0.105e)}}{1 + e^{0.05\pi \sin(0.105e)}}
\]  

where,

\[
e_1 = \begin{cases} 
0.105 & \text{if } 0.0105 + e > 0.2 \\
0.2 \sin(0.105e) & \text{if } 0.0105 + e \leq 0.2 
\end{cases}
\]

For the value of the non-linear function \( k(e) \) that can reach infinity, which will bring on the response of SVC that has an over value, the SVC control system voltage will be oscillating.

3.2 Improved SPX Algorithm

The \( K_p \) and \( K_i \) values of the non-linear PI Controller are optimized by improved SPX algorithm. The SPX algorithm of Nelder and Mead is a heuristic optimization method based on geometric considerations. The geometric figure whose vertices are defined by a set of \((n + 1)\) in an \( n \)-dimensional space is called a SPX. The basic idea in the SPX algorithm is to compare the values of the objective function at the \((n + 1)\) vertices of a SPX, not to seek the optimum point in a direction. The algorithm discards the worst vertex, (i.e.), highest value for a minimization problem and a new vertex is chosen gradually toward the optimum point during the iterative process [6, 7]. Moreover, it is adopted as the optimized objective function.

\[
\int_{0}^{t} f(x) dx
\]

Where the upper limit \( t \) is chosen as a finite time so that the integral can approach a steady-state value.

The convergence criterion of the SPX is presented as:

\[
\left| \frac{\int_{0}^{t} f(x) dx}{\int_{0}^{t} f_{\text{mean}}(x) dx} \right| < \varepsilon
\]  

Fig. 2. Control diagram of SVC

Fig. 3. Control block diagram of APF
4. Control method of APF

The overall control circuit of the shunt active filter is shown in Fig. 3. In this paper a new selective harmonic detection method is proposed. This can detect characteristic harmonics with precompensation of time delay. The selective harmonic detection method with pre-compensation technique is implemented here. In the selective harmonic detection method, the frequency of harmonic is achieved by Phase Locked Loop (PLL), and the amplitude of that is achieved in the rotary coordinate.

4.1 Reference current calculation

The reference current can be calculated using dq transformation. To solve the problem of time delay completely, the inverse transform matrix $C_n^*$ has been modified with $\Delta \phi_n$:

$$C_{dqa2abc} = \begin{bmatrix} \sin(\omega t + \Delta \phi_n) & -\cos(\omega t + \Delta \phi_n) \\ \cos(\omega t + \Delta \phi_n) & -\sin(\omega t + \Delta \phi_n) \end{bmatrix}$$

(5)

Where $\Delta \phi_n$ is the electric angle of the $n^{th}$ harmonic caused by time delay. The dc components $i_{dn}$ and $i_{qn}$ can be obtained though a low-pass filter. If the dc components $i_{dn}$ and $i_{qn}$ are calculated back to the abc-frame by the transform matrix $C^{-1} (\Delta \phi_n)$ and $C_{32}$, the $n^{th}$-order harmonic currents with pre-compensation can be obtained. After modification, the compensation current generated by APF will synchronize with the reference signal. The harmonic current compensation remainder rate will be small. If several order harmonics want to be detected at the same time, each order harmonic can be detected parallel. Then, the reference current can be obtained by adding them together. Then the harmonic current can be calculated by subtracting the reference current from the load current. The capacitor of the Shunt Active Filter can be maintained constant by using the PI controller. The simulation diagram for reference current calculation is shown in Fig. 4.

4.2 Improved Generalized Integrator Control

In this paper, an improved generalized integrator control (IGIC) was proposed to increase the performance of harmonic suppression [10]. IGIC is a PI controller used to eliminate error between the filter current and the harmonic current. It consists of several PI controllers. Each controller is tuned to reduce the particular harmonics. The structure of Improved Generalized Integrator Controller (IGIC) is shown in Fig. 5.
5. Simulation Results

5.1 Parameters of the simulation system

The parameters for the simulation circuit are shown in Table 1.

<table>
<thead>
<tr>
<th>System parameters</th>
<th>R/ohm</th>
<th>L/mH</th>
<th>C/µF</th>
</tr>
</thead>
<tbody>
<tr>
<td>System impedance</td>
<td>0.5</td>
<td>1</td>
<td></td>
</tr>
<tr>
<td>Load</td>
<td>10.6</td>
<td>58.2</td>
<td></td>
</tr>
<tr>
<td>Impedance SVC (TCR)</td>
<td>300</td>
<td></td>
<td></td>
</tr>
<tr>
<td>Coupling circuit (PPF)</td>
<td>0.1</td>
<td>20.71</td>
<td>478</td>
</tr>
<tr>
<td>Output filter</td>
<td>0.05</td>
<td>0.2</td>
<td>60</td>
</tr>
</tbody>
</table>

5.2 Simulation results without compensating device

Fig. 6(a). Waveform for load current (before compensation)

Fig. 6(b). Waveform for supply current (before compensation)

Fig. 7(a). Waveform for supply voltage (before compensation)

Fig. 7(b). Waveforms for supply voltage (before compensation)

Fig. 8. Spectrum analysis (before compensation)

The current and voltage waveforms (before compensation) are shown in Fig. 6 and Fig. 7. Due to non-linear load the supply and load currents contain harmonics so it becomes non-sinusoidal. The supply and load voltages are sinusoidal. The Total Harmonic Distortion of the supply current is 27.84%. The Total Harmonic Distortion analysis is shown in Fig. 8.

5.3 Simulation results (after compensation)

The compensating current generated by the Shunt Active Power Filter is shown in Fig. 9. The compensating current suppress the harmonic current drawn from the supply side and make current sinusoidal.

Fig. 9. Compensating current produced by SAPF

Fig. 10(a). Waveforms for supply current (after compensation)
After compensation the supply current become sinusoidal which can be shown in Fig. 10(a). The supply and load voltages after compensation is shown in Fig. 11(a) and Fig. 11(b). After compensation the supply voltage and load voltage are sinusoidal without any distortion.

The FFT analysis of the load current after implementation of the combined system is shown in Fig. 12. The Total harmonic distortion of the wave is 1.48%.

The simulated values of the three phase system with and without any compensating devices are shown in Table 2.

<table>
<thead>
<tr>
<th>System</th>
<th>Total Harmonic Distortion (%)</th>
<th>Power Factor</th>
</tr>
</thead>
<tbody>
<tr>
<td>Without compensating devices</td>
<td>27.84</td>
<td>0.7961</td>
</tr>
<tr>
<td>With combined system of SVC and APF</td>
<td>1.46</td>
<td>0.9393</td>
</tr>
</tbody>
</table>

After compensation the Total Harmonic Distortion of the supply current can be reduced to 1.48% from 27.84%. The power factor of the system without any compensating devices is 0.7961. SVC is the effective compensating devices. After implementation of the combined system the power factor can be improved to 0.9393.

The comparison of Harmonic orders for with and without any compensating devices is shown in Fig. 13. From the chart we conclude that the percentage of harmonics of each order can be reduced after the implementation of the combined system. In the combined system the TCR is connected in delta connection so the third order harmonics is zero. In this research work 5, 7, 9, 11 and 13 Order-harmonics are considered. The control methods implemented in this paper is more effective in the reduction of the harmonics.
6. Conclusion

In this research work, the combined system of a classical SVC and an APF has been tested and analyzed. The system has eliminated the harmonics generated by non-linear loads and thereby improved the power factor in the power system. The TCR in the SVC is star connected; hence the third order harmonics can be eliminated. Moreover, the active power filter topology has been adopted to suppress the harmonics generated by TCR and reduce the resonance between the grid and PPF. Separate control circuits for SVC and APF have been implemented in this work. The performance of the active power filter can be improved by using the combined system. Also, the harmonics can be reduced below 5% as per the IEEE standard.

References