SIMULATION AND EXPERIMENTAL ASSESSMENT OF POSITIVE OUTPUT TRIPLE LIFT LUO CONVERTER WITH DIFFERENT VARIOUS CONTROLLERS

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Abstract: The voltage lifting method is utilized in power electronic circuit. Applying this technique effectively overcomes the effects of parasitic elements and greatly increases the output voltage. Positive Output Triple-Lift Luo converters (POTLLC) are series of new DC-DC step-up converters; POTLLC circuit is derived from positive output elementary Luo converter by adding the lift circuit three times. These converters perform DC-DC voltage-increasing conversion with high power density, high efficiency and cheap topology in simple structure. TMS320C242 Digital Signal Processor has many special features to implement intelligent control algorithms in real time. Hence in this research work, design and hardware implementation of controllers have been carried out using TMS320C242 DSP for the POTLLC. The simulation and experimental results are presented and the performance evaluation of the PI, Fuzzy and Neural controller for Triple-Lift Luo Converter is compared under supply voltage disturbance load disturbances.

Keywords— Fuzzy logic controller, Positive output Triple-Lift Luo converter, PI controller, Neural controller.

1. Introduction.

DC-DC converters accept DC input voltage at one level and produce DC output voltage at another level [1-5]. Voltage Lift technique is applied in the periodical switching circuit. Usually, a capacitor is charged during switch-on by source voltage, this charged capacitor voltage is the output voltage during switch-off period. For DC-DC converters with constant output voltage, it is always desirable that the output voltage remains unchanged in both steady state and transient operations whenever the supply voltage and/or load current are disturbed. DC-DC converters are generally divided into two groups: hard switching converters and soft-switching converters. In hard-switching converters, the power switches cut off the load current within the turn-on and turn-off times under the hard switching conditions. The output voltage is controlled by adjusting the on time of the power switch, which in turn adjusts the width of a voltage pulse at the output. This is known as PWM control. The commonly used control methods for DC-DC converters are pulse width modulated (PWM) voltage mode control, PWM current mode control and PID controller. These conventional controllers are unable to perform satisfactorily under large parameter or load variation. Fuzzy logic control and neuro control are work very well for nonlinear, time variant and complex systems, this research work presents the control of positive output Triple-Lift Luo Converter using FLC. Neural controllers and compared with PI controller [6-15].


The POTLLC circuit is shown in Fig.1. Switches are power MOSFET device. They are driven by a pulse-width-modulated (PWM) switching signal with
repeating frequency $f$ and conduction duty $k$. The switch repeating period is $T = 1/f$, so that the switch-on period is $kT$ and switch-off period is $(1-k)T$.

The load is resistive, the combined inductor $L = L_1 + L_2$ (L1 + L2); the normalized load is $Z_L = RL/L$. The converter consists of a pump circuit S–L1–C–D and a low-pass filters L2, C0 and lift circuit. The pump inductor L1 transfers the energy from the source to capacitor C during switch-off and then the stored energy on the capacitor C is delivered to load R during switch-on. Therefore, if the voltage $V_o$ should be correspondingly higher. When the switch S turned off, the current $i_0$ flows through the free-wheeling diode D. This current descends in whole switching-off period $(1-k)T$. If current $i_0$ does not become zero before switch S turned on again, this working state is defined as continuous mode. If current $i_0$ becomes zero before switch S turned on again, this working state is defined as discontinuous mode. The triple-lift LUO circuit consist of two static switch S and S1, four inductors L1, L2, L3 and L4, five capacitors, C1, C2, C3 and C0, and five diodes. Capacitors C1, C2, and C3 perform characteristic functions to lift the capacitor voltage $V_C$ by three times of source voltage $V_L$, $L_1$ and $L_4$ perform the function as ladder joints to link the three capacitors C1, C2, and C3 and lift the capacitor voltage $V_C$ up. Current $i_{L1}(t)$, $i_{C1}(t)$, $i_{C2}(t)$ are exponential functions. They have large values at the moment of power on, but they are small because $V_{C1} = V_{C2} = V_{C3} = V_I$ in steady state. The circuit parameters of the chosen Luo converter is listed in Table I.

The output voltage and current are

$$V_o = \frac{3}{1-k}V_I \quad \text{and} \quad I_o = \frac{3}{1-k}I_I$$

The Voltage transfer gain in continuous mode is

$$M_T = \frac{V_o}{V_I} = \frac{3}{1-k}$$

Other average voltages:

$V_{C1} = V_{C2} = V_{C3} = V_I$

Other average currents:

$$I_{L2} = I_0 \quad \text{and} \quad I_{L4} = \frac{k}{1-k}I_0$$

$$I_{L3} = I_{L4} = I_{L2} + I_{L2} = \frac{1}{1-k}I_0$$

Fig.1. Positive output Triple –Lift Luo Converter.

<table>
<thead>
<tr>
<th>Parameters</th>
<th>Symbol</th>
<th>Values</th>
</tr>
</thead>
<tbody>
<tr>
<td>Input voltage</td>
<td>$V_{in}$</td>
<td>10 V</td>
</tr>
<tr>
<td>Output voltage</td>
<td>$V_o$</td>
<td>60V</td>
</tr>
<tr>
<td>Inductors</td>
<td>$L_1$–$L_2$–$L_3$–$L_4$</td>
<td>330µH</td>
</tr>
<tr>
<td>Capacitors</td>
<td>$C_0$–C1–C2–C3–C</td>
<td>22µf/60V</td>
</tr>
<tr>
<td>Load resistance</td>
<td>R</td>
<td>10Ω</td>
</tr>
<tr>
<td>Switching frequency</td>
<td>$f_s$</td>
<td>50KHZ</td>
</tr>
<tr>
<td>Duty ratio</td>
<td>$D$</td>
<td>0.5</td>
</tr>
</tbody>
</table>

3. Design of PI controller.

The function of a PI controller is to receive the actual output voltage from the converter is measured and compares it with the reference voltage and to produce the error signal so as to drive the converter to the desired value. The main function of PI controller is to reduce the peak overshoot and make steady state error zero. PI controller settings $K_p$ and $T_i$ are designed using Ziegler –Nichols tuning technique based on the converter’s open loop step response. Converters are modeled using the MATLAB-SIMULINK and PI control is developed using the control system toolbox. Errors in the output voltage and duty cycle of the MOSFET are respectively the input and output of the PI controller.

4. Design of fuzzy logic controller.

The block diagram of the fuzzy logic control scheme for the POTLLC is shown in Fig.2. The output voltage of the Luo converter is compared with the reference voltage. After comparison, the error (e) and the change in error (ce) are calculated and are given as inputs to the fuzzy controller. In this work, the error is normalized to a per-unit value with respect to the reference voltage, which helps in using the fuzzy controller for any reference voltage. The fuzzy controller will attempt to reduce the error to zero by changing the duty cycle of switching signal. The fuzzy controller is divided into five modules: fuzzifier, data base, rule base, decision maker and defuzzifier. Various steps in the design of FLC for chosen Luo converter are stated below:
FLC uses linguistic variables instead of numerical variables. The process of converting a numerical variable (real number or crisp variable) into a linguistic variable (fuzzy number) is called fuzzification. In the present work, the error and change in error of voltage are fuzzified. Seven linguistic fuzzy sets with triangular membership function are as shown in Fig. 3. The seven fuzzy variables for ‘error’, ‘change in error’ and change in the duty cycle are Negative Big (NB), Negative Medium (NM), Negative Small (NS), Zero (Z), Positive Big (PB), Positive Medium (PM) and Positive Small (PS).

**A. Fuzzification**

The FLC produces the required output in a linguistic variable (fuzzy number). According to real-world requirements, the linguistic variables have to be transformed to crisp output. Center of gravity method is used for defuzzification in this work. The defuzzified output is the change in duty cycle.

$$d\delta = \sum_{i=1}^{4} w_i m_i$$

**5. Design of neural controller.**

Considering the inherent nonlinearity of the Luo converter, the output dependence of the circuit parameters that can change continuously and the demands on regulation and response time normally required for a power supply, it is clear that the design based on linear models does not meet the requirements. Artificial neural networks have many characteristics similar to the human brain are capable of learning from experience, generalization, abstracting essential characteristics from inputs high tolerance to faults, real time operation, etc. Therefore, neural networks offer many advantages for the control of Luo converter. The actual output voltage is fed back and is compared with reference voltage. After comparison, error and the change in error are calculated and are given as input to the controller. The neural controller attempts to reduce the error to zero by changing the duty cycle of switching signal.

MATLAB/Simulink model of the Triple-Lift Luo converter was developed and simulated with Fuzzy Logic Controller using Fuzzy Tool Box. From the simulation, error, change in error and duty cycle was acquired. These data were used to train the neuro controller. Then the closed loop operation was simulated with neuro controller using MATLAB NN Tool Box to achieve the desired performance. In this work Quasi-Newton back-propagation algorithm is employed to update weights Mean Square Error (MSE) is the performance criterion that evaluates the network according to the mean of square of error between the target and computed output. LEARNGD learning function which has the gradient descent with momentum weight / bias learning function has been used in this work. Learning occurs according to the learning parameters. The activation functions are bipolar sigmoid type and linear activation function are used for hidden and output.
layers respectively. There is no general procedure to determine the exact size of the neural network. However, the size of the network developed in this work showed itself satisfactory as far as the output voltage regulation is concerned. Trials have been carried out to obtain maximum accuracy with minimum number of neurons per layer.

Fig. 5. Block Diagram of Neuro for Luo converter.

6. Simulation and hardware results.

Fig.6 shows the measured responses of the output voltage with PI controller when the supply voltage is changed to ±25% of rated voltage at 0.035sec and 0.07sec. For the supply change from 10V to 12.5V and \( R = 10\Omega \), the output voltage is regulated within 6msec and the %peak overshoot is 10. When the supply voltage is changed from 12.5V to 10V, the settling time is 8msec with 8.33% peak overshoot.

Fig. 6. Line regulation of POTLLC with PI controls Step change of supply voltage from 10-12.5V at 0.035sec and 12.5-10v at 0.07sec.

Fig.7 shows the start up as well as transients of the converters with fuzzy controller under small signal step disturbances in supply. A 25% step increase in the input voltage and vice versa applied at t=35msec and t=70msec, the line disturbances are rejected within 3msec for a step change of 10V-12.5V and 7msec for a step change of 12.5V-10V. The peak overshoots are 8.33% and 5.83% for ±25% step change in the rated supply voltage. For the neuro controller Fig.8, it can be seen that for the input supply voltage stepping-up from 10V to 12.5V (25% of rated supply voltage) at 0.035sec, the %peak overshoot and settling time are 8.03 and 3msec and for the supply stepping down from 12.5V to 10V (25% decrease of rated supply voltage) at 0.07sec, the %peak overshoot and settling time are 3.33 and 4msec.

Fig. 7. Line regulation of POTLLC with Fuzzy controller Step change of supply voltage from 10-12.5V at 0.035 sec and 12.5-10v at 0.07sec.

Fig.8. Line regulation of POTLLC with neuro controller: Step change of supply voltage from 10-12.5V at 0.035 sec and 12.5-10v at 0.07sec.

Fig.9 shows the output voltage of the converter with PI controller with a step change of ±20% of rated load at 0.035 sec and at 0.07 sec. It can be seen that the %peak overshoot is 7.5 and the settling time is 6msec for a step change of 10-12Ω and step change of 12-10Ω, the %peak overshoot is 6.66 and the settling time is 7msec.

Fig.10 shows the closed loop response of Triple-Lift Luo converter with fuzzy controller for sudden disturbances of 20% of rated load. The output voltage is regulated within 3msec and the peak overshoot is 5% for a step change of load from 10-12Ω. The settling time is 6msec and the peak overshoot is 5.83% for a step change of load from 12-10Ω.

Fig.9. POTLLC under load regulation with PI control: Step change of resistance from 10-12Ω at 0.035 sec and 12-10Ω at 0.07sec.
Fig. 11 shows the output voltage of the Luo converter with neuro controller for a step change of ±20% of rated load at 0.035sec and at 0.07sec. It can be seen that the %peak overshoot is 4.1 and the settling time is 2msec for a step change of 10 -12 Ω. The %peak overshoot is 3.3 and settling time is 2msec for a step change of 12 – 10 Ω.

Fig. 10. POTLLC under load regulation with Fuzzy controller: Step change of resistance from 10-12Ω at 0.035 sec and 12-10Ω at 0.07sec.

Fig. 11. POTLLC under load regulation with neuro controller: Step change of resistance from 10-12Ω at 0.035 sec and 12-10Ω at 0.07sec.

Fig. 12 and 13 show the line regulation and load regulation of POTLLC with PI, fuzzy and neuro controllers.

Fig. 12. Closed loop responses of POTLLC with various controllers under line variations.

Fig. 13. Closed loop responses of POTLLC with various controllers under load variations.

The block diagram for the TMS320C242 DSP based implementation of closed loop control of a triple-lift Luo converter is shown in Fig. 14. The output voltage of the converter is scaled down to 0–5volts and read by the 10-bit ADC of DSP. The DSP executes 20 MIPS with 50 ns instruction cycle time. The conversion time of the on-chip ADC is 1µs. The DSP takes an average of 500µs to execute the fuzzy logic control algorithm, which involves sampling the output voltage, calculating the new duty cycle and updating the PWM output.

Fig. 14. Block diagram DSP based implementation of closed loop control of a triple-lift Luo converter.

The switching device S1 used is a N-channel MOSFET (enhancement type) IRF540N and S is a P-channel MOSFET IRF9630. In order to provide isolation between the Triple-Lift Luo converter circuit and the DSP, the isolation amplifier HCPL7840 is needed in the feedback path. The optocoupler MCT2E provides the isolation between the DSP and MOSFET of the Triple-Lift Luo converter. The PWM signal from the DSP is not capable of driving MOSFET. In order to strengthen the pulses, MOSFET driver IC IR2110 is used. A snapshot of the experimental setup for a Luo converter is displayed in Fig. 15. Fig. 16 shows the output voltage for the Luo converter with PI controller for a step change of ±25% of rated supply voltage at 0.04sec and at 0.07sec. The experimental results show that the output voltage is regulated within a maximum of 12msec after line disturbances and the %peak overshoot is 10.05. The disturbance rejection of the fuzzy control is validated by the input voltage variation from 10V to 12.5V at t = 0.04sec (Fig. 17). The output voltage is...
compensated within 5.2msec and the peak overshoot is 10%. For the step change in the supply voltage from 12.5V to 10 V at 0.07sec, the output voltage reaches the reference voltage within 5.5msec and peak overshoot is 8.2%. Fig.18, shows the experimental output voltage of the Luo converters with neuro controller under line disturbance. From the Fig.18, it can be seen that the input supply voltage was stepping-up from 10V to 12.5V (25% of rated supply voltage) at 0.04sec. The %peak overshoot and settling time are 8.16 and 4msec and stepping down from 12.5V to 10V (25% decrease of rated supply voltage) at 0.07sec. The %peak overshoot and settling time are 3.6 and 4.25 msec.

Fig.15. Hardware set up for Triple –Lift Luo converter.

Fig.16. Hardware output of Line regulation of POTLLC with PI control: Step change of supply voltage from 10-12.5V at 0.035sec and 12.5- 10v at 0.07sec.

Fig.17. Hardware output of Line regulation of POTLLC with fuzzy control: Step change of supply voltage from 10-12.5V at 0.035sec and 12.5- 10v at 0.07sec.

Fig.18. Hardware output of Line regulation of POTLLC with neuro control: Step change of supply voltage from 10-12.5V at 0.035sec and 12.5-10v at 0.07sec.

Fig.19 shows the output voltage of the Luo converter with PI controller for a step change of ±20% of rated load at 0.04sec and at 0.07sec. It can be seen that the %peak overshoot is 8.16 and the settling time is 5.1msec for a step change of 10 -12 Ω and 8.50 and 4.65msec for a step change of 12 – 10 Ω. For the load variation from 10 Ω to 12 Ω at t=0.04sec the output voltage of the converter with fuzzy controller is compensated within 4 msec and the %peak overshoot is 11.5 as shown in Fig.20. For the load of variation of 12 Ω to 10 Ω at t = 0.07sec, the output voltage is regulated within 3.92msec and the %peak overshoot of 9.12. Fig.21 shows the output voltage of the Luo converter with neuro controller for a step change of ±20% of rated load at 0.04sec and at 0.07sec. It can be seen that the %peak overshoot is 5.83 and the settling time is 3.05msec for a step change of 10 -12 Ω. The %peak overshoot is 5.33 and settling time is 2.89msec for a step change of 12 – 10 Ω.

Fig.19. Closed loop responses of positive output Triple-Lift Luo converter with PI control under sudden disturbances of ± 20% of rated load.

Fig.20. Closed loop responses of positive output Triple-Lift Luo converter with fuzzy control under sudden disturbances of ± 20% of rated load.

Fig.21. Closed loop responses of positive output Triple-Lift Luo converter with neuro control under sudden disturbances of ± 20% of rated load.
Table III Performance comparison of simulation and experimental results for positive output Triple – Lift Luo converter

<table>
<thead>
<tr>
<th>Controller</th>
<th>Start up Transient</th>
<th>Supply Disturbances</th>
<th>Load Disturbances</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>Delay time (ms)</td>
<td>Rise time (ms)</td>
<td>Peak over shoot (%)</td>
</tr>
<tr>
<td>PI</td>
<td>2</td>
<td>7</td>
<td>0</td>
</tr>
<tr>
<td>Fuzzy</td>
<td>2</td>
<td>6</td>
<td>0</td>
</tr>
<tr>
<td>Neuro</td>
<td>2</td>
<td>7</td>
<td>0</td>
</tr>
<tr>
<td>PI</td>
<td>3</td>
<td>5</td>
<td>9.16</td>
</tr>
<tr>
<td>Fuzzy</td>
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<td>5</td>
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</tr>
<tr>
<td>Neuro</td>
<td>3</td>
<td>8</td>
<td>0</td>
</tr>
</tbody>
</table>

7. Conclusions

From table III, Positive output Triple-Lift Luo converters with PI, FLC and ANN controllers are analyzed. The experimental results confirm that intelligent controllers rejects both line and load disturbances. Also the results proved that neuro controller gives the smooth response for both line and load disturbances according to the desired voltage. Using the above controllers, stable and zero ripple output voltage of the Triple-Lift Luo converter is obtained.

References


